#### **Performance Testing --- Update**

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### **Regional Effort**

- Look at lab performance of typical mixes from the region (|E\*| and flow number)
- Compare with SST results (FS and RS)
  - Seven conventional Superpave mixes (one with 15% RAP)

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- One Marshall mix
- Three SMA mixes

#### **Mixes Tested**

Mix ID	Binder	N <sub>des</sub>	NMAS	T <sub>eff</sub> °C
IA	PG64-22	109	12.5 mm	39.1
KS	PG64-22	75	9.5 mm	40.4
MO	PG70-22	125	12.5 mm (c)	41.8
M	PG58-28	76	9.5 mm (f)	34.2
MN	PG64-22	100 🗉	12.5 mm (f)	36.9
MN-M	PG64-28	75 blows	Minus 3/4"	36.9
WI1	PG70-28	100	12.5 mm	34.0
WI2	PG58-28	100	12.5 mm	34.0

# **Mixes Tested -- SMA**

Mix ID	Binder	N <sub>des</sub>	NMAS	T <sub>eff</sub> °C
IN1	PG76-22	100	9.5 mm	38.4
IN2	PG70-28	100	12.5 mm	39.6
MOSM	PG70-22	100	12.5 mm	41.1

• WI1 and WI2 also tested in confined mode

#### **12.5 mm NMAS**



#### 9.5 mm NMAS



#### **Tests Conducted**

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5	Test Method	T°C	
	Frequency Sweep	T <sub>eff</sub> []	54.4
	Repeated Shear		58.0
	Dynamic Modulus	T <sub>eff</sub>	54.4
	Dynamic Creep	T <sub>eff</sub>	

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# **Superpave Shear Tests**

Frequency sweep (10 Hz - 0.01 Hz)
Apply sinusoidal shear strain (0.01%)

- Measure axial and shear load and deformations
- Determine  $|G^*|$  and  $\delta$





Repeated shear
Apply shear stress (69 kPa for 0.1 s with 0.6 s rest period)
Measure cumulative shear deformation
5000 cycles or 5% strain



#### **Superpave Performance Tests**

Dynamic modulus (25 Hz to 0.1 Hz)

- Apply cyclic haversine loading
- Axial strains limited to 50 150  $\mu\epsilon$
- Determine  $|E^*|$  and  $\delta$



#### **Superpave Performance Tests**



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#### Dynamic creep

- Apply cyclic pulses;100 ms pulse width with 900 ms rest period
- 5% axial strain or 15000 cycles
- Determine flow number

# **Performance Testing ---- Update** RESULTS

**Frequency Sweep Data** 



# Frequency Sweep Data

- Mixes significantly different
- Minnesota Marshall mix was too soft to be tested at 54.4°C
- At  $T_{\rm eff}$  WI1 and MO were statistically similar
- At 54.4°C, mixes showed overlapping groups
- At T<sub>eff</sub>, all three SMA mixes were statistically different; but not at 54.4°C



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- Mixes significantly different
- Mixes with similar gradation, but different binder grades
  - MI and KS --- mix with softer binder showed lower modulus at higher test temperature
  - WI1, WI2, MN and MNM --- mix with stiffest binder (WI1) had highest modulus
    - WI2 with softest binder (PG58-28) performed better than Marshall mix with PG64-28
    - MO mix ranked low in DM; unlike that observed in FS



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#### Mixes significantly different

- IN2 with PG76-22 has the lowest stiffness under confined test conditions at both temperatures
- Modulus of conventional mixes was higher than (or was comparable to) that of SMA mixes
- Modulus of WI2 with PG58-28 binder was comparable to SMA mixes (MOSM, IN1) with stiffer binder grades (PG70-22 and PG70-28, respectively)

# **Mix |E\*| vs. |G\*|**



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# **Confined vs. Unconfined**



# **Confined vs. Unconfined**

• WI1 and WI2 -- Different binder grades Modulus of WI1 versus WI2 (confined) • Significant diff. in mean modulus at both test temperatures Modulus of WI1 versus WI2 (unconfined) Significant diff. in mean modulus at both test temperatures Modulus of confined versus unconfined samples For both WI1 and WI2 mixes No significant differences at T<sub>eff</sub> Significant differences at 54.4°C

#### **Repeated Shear Data**



# **Repeated Shear Data**

- All tested at 54.4°C
- Minnesota Marshall mix and Kansas mix exhibited poor rut resistance (4.3% strain)
- Indiana SMA mixes showed the lowest amount of cumulative strain overall
- Curiously, WI1 (PG70-28) showed higher cumulative strain than WI2 (PG58-28)
- WI2 mix outperformed KS and MNM mixes -- aggregate structure contribution to rut resistance more dominant

## **Dynamic Creep Data**

Mix ID	Binder	T <sub>eff</sub> °C	Flow #
IA	PG64-22	39.1	14767
KS	PG64-22	40.4	13044
МО	PG70-22	41.8	10484
MI	PG58-28	34.2	2183
MN	PG64-22	36.9	9898
MN-M	PG64-28	36.9	9795
WI1	PG70-28	34.0	11423
WI2	PG58-28	34.0	13307
MOSM	PG70-22	38.4	4458
IN1	PG76-22	39.6	14783
IN2	PG70-22	41.1	8381

# **Dynamic Creep Data**

- Flow number -- No. of cycles at start of flow
- As in the case of repeated shear testing, WI2 showed better performance than WI1 under repeated load conditions
- In general, conventional mixes performed better than SMA mixes
- IA and IN1 ranked the highest; followed by KS and WI2 (but at diff. test temperatures)
- IA and IN1 also performed well in RS testing; but KS was ranked lowest in RS testing

# **Dynamic Creep Data**

- Minnesota Marshall and Superpave mixes showed similar flow numbers
- MI and MOSM mixes ranked the lowest
- Overall, no good correlation between repeated shear test results and dynamic creep test results

#### Conclusions

- Good comparison b/w FS and DM test results.
- Poor correlation b/w RS and DC test results
- In general, conventional mixes had higher modulus than SMA mixes
- WI1 performed well in all four tests.
- MO mix designed for higher traffic volume showed high modulus in shear modulus testing, but not in dynamic modulus testing
- Influence of confinement on dynamic modulus more evident at higher temperatures